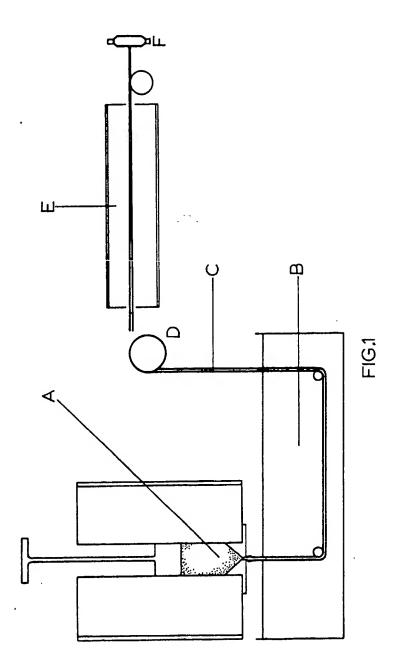
(12) UK Patent Application (19) GB (11) 2 042 414 A

- (21) Application No 8004157
- (22) Date of filing 7 Feb 1980
- (30) Priority data
- (31) 7900990
- (32) 8 Feb 1979
- (33) Netherlands (NL)
- (43) Application published 24 Sep 1980
- (51) INT CL3 D01D 5/04
- (52) Domestic classification **B5B** 350 352 353 35Y 360 361 363 367 AH
- (56) Documents cited GB 1541941 GB 1517610 GB 1295183 GB 1049696 GB 985718 GB 582013
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(54) Dry-spinning polymer filaments

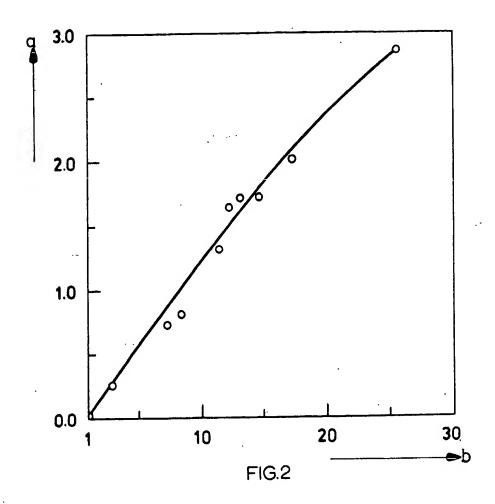
(57) A process for making polymer filaments which have a high tensile strength and a high modulus by stretching a polymer filament which contains a substantial amount, eg at least 25 wt % of polymer solvent at a temperature between the swelling point and the melting point of the polymer. A solution of the polymer may be spun to a filament through a spinning aperture and the spun filament cooled to below the dissolution temperature of the polymer without substantial evaporation of solvent from the filament and then brought to a temperature between the swelling point and the melting point of the polymer, and stretched. By the process polyethylene filaments may be obtained having a tensile strength of at least 1.2 GPa.

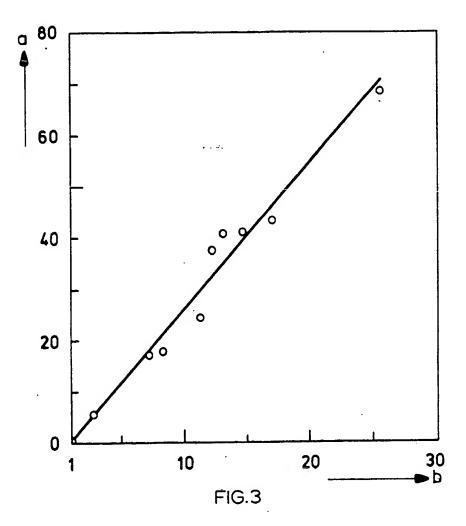


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SPECIFICATION

Filam nts of high tensile str ngth and m - dulus

This invention relates to polymer filaments of high tensile strength and modulus, and to a process of making such filaments by spinning a solution of spinnable polymer material.

10 Filaments are made by spinning linear polymers in liquid form, i.e. as a melt or solution. The randomly oriented chains of molecules in the filament thus obtained are then oriented lengthwise in the filament by stretch-15 ing. Although also other substances may be capable of being spun, the chain-formed macromolecules are an important condition of their capability of being spun into filaments. Side branches have an adverse effect on fila-20 ment formation and mechanical properties... Therefore the production of polymer filaments utilizes polymers that are substantially linear. although a limited degree of branching will in most cases be unavoidable, and allowable.

By stretching the filaments, the chain macromolecules are oriented lengthwise and the strength of the filaments increases. However in many instances the strength remains far below the value that is theoretically possible.
Many attempts have previously been made at producing filaments the tensile strength and modulus of which come closer to what is theoretically possible, as described in the publication by Juyn in Plastica 31 (1978)

35 262-270 and Bigg in Polymer Eng. Sci. 16 (1976) 725-734 and have failed to yield satisfactory results. In a number of instances it was possible to sufficiently improve the modulus but not the tensile strength, but the 40 filament formation is so slow that economic production is impossible.

It has now been found that polymer filaments of high tensile strength and modulus can be made by stretching a polymer filament containing a substantial proportion of polymer solvent, at a temperature between the swelling point and the melting point. Preferably a solution of a spinnable polymer is spun through a spinning aperture and the spun filament is cooled below the dissolution temperature of the polymer without substantial evaporation of solvent from the filament and is then heated to a temperature between the swelling point of the polymer in the solvent and the melting point of the polymer, and is streched.

In the process called dry spinning, a generally know process applied on a t chnical scale, a solution of a spinnable polymer is 60 spun in a shaft through which—usually heated—air is blown to evaporate all or most of the solvent from the filament. The temperature in the shaft is below the multing point of the polymer, so that this is precipitated when 65 the solvent is vaporated. This increases the

mechanical strength of the filament, which is still very low at the exit through the spinning aperture. The strength is further increased in the following stretching operation at tempera-

70 tures below the melting point of the polymer. According to the present invention, the evaporation of the solvent from the filament immediately after spinning is not promoted during the cooling phase. The filament can be

75 cooled to below the solution temperature, and particularly to below the swelling point of the polymer in the solvent, in any suitable way, for instance by passing the filament into a water bath, or through a shaft, with no or

80 hardly any air being blow through this shaft. Some evaporation of the solvent from the filament will often take place spontaneously and not be preventable. This does not do the least harm, as long as the evaporation is not

85 actively promoted and the amount of solvent in the filament is not reduced to a low value, e.g. to less than 25% by wt. of solvent relative to the polymer, preferably not to less than equal amounts (100%) by weight of

90 solvent and polymer. If so desired, evaporation of the solvent may be reduced or suppressed by carrying out the spinning in an atmosphere containing solvent vapour.

In cooling to below the solution tempera-95 ture, in particular to below the swelling temperature of the polymer in the solvent, the polymer precipitates from the solution, and a gel is formed. A filament consisting of this polymer gel has sufficient mechanical strength

100 for further processing, e.g. by means of the guides, rolls, etc., customarily used in spinning techaniques. A filament of this kind is heated to a temperature between the swelling point of the filament in the solvent and the

105 melting point of the polymer, and stretched at that temperature. This can be effected by passing the filament into a zone containing a gaseous or liquid medium kept at the required temperature. A tubular oven with air for the

110 gaseous medium is very suitable, but it is also possible to use a liquid bath or any other suitable device. A gaseous medium is easier to handle, and deserves preference.

When the filament is being stretched, sol-115 vent evaporation, or—if a liquid medium is used—dissolution of solvent in the liquid will occur. By preference, evaporation is promoted by adequate measures, e.g. removal of the solvent vapour, for instance by leading a gas

120 or air current past the filament in the stretching zone. At least part of the solvent should be evaporated, but by preference at least the greater part of the solvent is evaporated, so that at the end of the stretching zon at most

125 a small amount—e.g. not more than a few per cent, calculated on a solid-substance basis—of solvent is contained in the filament. The filament eventually obtained must be free of solvent, and it is advantageous to apply such
130 conditions that it is free, or virtually free, of

solvent already in the stretching zone.

Surprisingly, the process according to the invention can produc filaments that are considerably stronger than filaments of the same material made by any of the usual dry spinning processes, that is to say, filaments of considerably higher tensile strength and modulus. By means of the methods described in the abovementioned publications by Juyn and Bigg filaments of higher modulus have been made, admittedly, but the tensile strength still leaves much to be desired. Moreover, the productivity of these methods is low.

The process according to the invention differs from the usual dry spinning processes in that a filament containing an appreciable amount of solvent for the spinnable material is stretched at a temperature at which the spinnable material will at least swell in the solvent, with removal of the solvent, whereas in the usually applied spinning processes solvent-free filaments are subjected to stretching.

A requirement of dry spinning is that the linear polymer be soluble in a suitable solvent.

For any soluble polymer a number of solvents are known. The expert can without any difficulty select therefrom a suitable solvent whose boiling point is not so high as to make it difficult for the solvent to be evaporated from the filament, and not so low as to make it too volatile and hinder filament formation on account of rapid evaporation, or has to be used under pressure to prevent this.

Dissolution of a polymer in a suitable sol-35 vent involves swelling. Whilst solvent is absorbed and the volume increases, a strongly swollen gel is formed, which however, on account of its consistency and stability of shape still has to be regarded as a kind of 40 solid substance. It is generally assumed that the polymer is composed of ordered (crystalline) and less ordered (amorphous) area. The ordered areas are believed to act as anchoring points and thus lend stability of shape to the 45 gel. The formation of the gel and the dissolution are time-dependent. A given polymer can be dissolved in a given solvent only above a given temperature. Below this dissolution temperature only swelling takes place, and ac-50 cording as the temperature is lower, the swelling becomes less, until at a certain point it is negligible. The swelling point or swelling temperature is considered to be that temperature at which a distinct increase in volume and a 55 distinct absorption of solvent-5 to 10% of

lymer.
In dry spinning processes as usually applied, mostly 5–30% wt. solutions are used, for technical and conomic reasons. Such 65 solutions are suitable also for the pr s nt

60 questionably absorbed into the swelling po-

the polymer weight---occur. For the sake of

simplicity, the swelling temperature above which the stretching is to be ffected is th

temperature at which 10% of solvent is un-

process, although in general use will be made of solutions of lower concentration. Advantageously, us is made of 1–5% wt. solutions. Still low r concentrations can sometimes be 70 applied, although these do not present advan-

tages and are economically disadvantageous.
Suitable stretching ratios can be easily determined by experiment. Tensile strength and modulus of the filaments are, within certain

75 limits, about proportional to the stretching ratio. According as the filaments should be stronger, a greater stretching ratio will have to be chosen.

The stretching ratio is at least 5, by prefer-80 ence at least 10, more in particular at least 20. High stretching ratios, 30 to 40 and even higher, can be applied without objection, and give filaments whose tensile strength and modulus are appreciably higher than those of 85 filaments made by the usual processes.

In dry spinning processes as usually applied, the diameters of the spinning apertures in the spinning nozzles are usually small. In general, these diameters are 0.02-1.0 mm.

90 Especially if small spinning apertures (≤0.2 mm) are used, the spinning process proves highly sensitive to the presence of impurities in the spinning solution, so that this should be carefully freed and kept free of solid impuri-

95 ties. In most cases, filters are placed on the spinning nozzles. In spite of this, it appears that the spinning nozzles need to be cleaned after a short time, and blockage still occurs frequently. In the present process larger spin-

100 ning apertures, of more than 0.2 mm, e.g. 0.5 to 2.0 mm or more, can be used, since considerably higher stretching ratios can be applied and, in addition, generally lower polymer concentrations in the spinning solution 105 are applied.

The invention is not restricted to the production of strong filaments of certain polymers, but can be generally used for materials that can be dry-spun to filaments.

110 Polymers that can be spun by the process according to the present invention are, for instance, polyolefins such as polyethylene, polypropylene, ethylene-propylene copolymers, polyoxymethylene, polyethylene oxide, poly-

115 amides, such as the various types of nylon, polyesters, such as polyethyleneterephtalate, polyacrylonitrile, vinyl polymers such as polyvinylalcohol, polyvinylidenefluoride.

Polyolefins such as polyethylene, polypropy-120 lene, ethylenepropylene copolymers and higher polyolefins can without objection be dissolved in hydrocarbons such as saturated aliphatic and cyclic, as well as aromatic hydrcarbons, or mixtures there is such as mineral

125 oil fractions. Very suitabl are aliphatic or cyclic hydrocarbons such as nonane, decane, undecane, dodecane, tetralin, decalin, etc., or mineral oil fractions corresponding in boiling range. Polyethyl ne or polypropylen is pr f-1.30 erably dissolved in decalin or dodecane. The

present method is particularly suitable for th preparation of filaments of polyolefins, preferably polyethylene having a tensile strength of at least 1.2 GPa.

It is also possible to make filaments of solutions of two or more polymers in a common solvent by the present process. For this purpose the polymers need not be miscible with each other. For instance, it is possible to 10 dissolve together in decalin or dodecane polyethylene and polypropylene, whose melts are immiscible, and to spin the solutions thus obtained.

The filaments according to the invention 15 can be used for many purposes. They can be applied as reinforcement in many kinds of materials for which reinforcement with fibres or filaments is known, for tyre yarns, and for all possible applications in which low weight 20 combined with high strength is a desirable feature. As a matter of course, the range of possible application is not limited to those mentioned above.

The invention will be elucidated by means 25 of the following examples, without being restricted thereby.

Example 1

A polyethylene of high molecular weight, 30 with $\overline{M}_{w} \simeq 1.5 \times 10^{6}$, was dissolved in decalin at 145°C to form a 2% wt. solution. This solution A was spun through a spinning nozzle with a spinning aperature of 0.5 mm dia., at 130°C. The filament was passed into 35 a water bath B kept at room temperature, where it was cooled. The cooled, 0.7 mm thick filament C, which was gel-like in appearance and still contained about 98% solvent, was next passed over feed reel D through a 40 tubular oven E heated at 120°C, and stretched over stretching reel F, with the use of various stretching ratios. This process is shown in diagram in Fig. 1.

Figs. 2 and 3 show, respectively, the ten-45 sion strength and the modulus a plotted against the stretching ratio b. A modulus of more than 60 GPa and a tensile strength of almost 3 can be attained, whereas the modulus of polyethylene filaments made in the 50 conventional way is 2-3 GPa, and the tensile strength about 0.1 GPa. The values of modulus and tensile strength of filaments made with different stretching ratios as plotted in Figs. 2 and 3 are mentioned in Table 1.

Polyethylene filaments having a tensile strength of over 1.2 GPa can easily be produced by means of the present process.

Table 1

70	Expt.	Stretching ratio	Modulus, GPa	Tensile strength GPa
, ,	1	1	2.4	0.09
	2	3	5.4	0.27
	3	7	17.0	0.73
75	4	8	17.6	0.81
	5	11	23.9	1.32
	6	12	37.5°	1.65
	7	13	40.9	1.72
	8	15	41.0	1.72
	9	17	43.1	2.11
80	10	25	69.0	2.90
	11	32	90.2	3.02

Example 2

According to the process described in Ex-85 ample 1, a 2% wt. solution of a mixture of equal parts of high-molecular-weight polyethylene, with $\overline{M}_{w} \approx 1.5 \times 10^{6}$, and a highmolecular-weight polypropylene, with M_w ~ 3.0 × 106, was spun at 140°C and stretched 90 at 130°C, using a stretching ratio of 20. The filaments had a tensile strength of 1.5 GPa.

Example 3

According to the process described in Ex-95 ample 1, a 2% wt. solution of isotactic polypropylene, with $\bar{M}_{\rm w} \simeq 3.0 \times 10^6$, was spun at 140°C and stretched at 130°C, using a stretching ratio of 20. The tensile strength of the resulting filaments was 1 GPa.

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CLAIMS

- A process for making polymer filaments of high tensile strength and modulus, characterized in that a polymer filament containing a 105 substantial proportion of solvent for the polymer is stretched at a temperature between the swelling point and the melting point of the polymer.
- 2. A process according to Claim 1, charac-110 terized in that a solution of the polymer is spun to a filament through a spinning aperture and the spung filament is cooled to below the dissolution temperature of the polymer without substantial evaporation of sol-
- 115 vent from the filament and is then brought to a temperature between the swelling point and the melting point of the polymer, and is stretched.
- 3. A process according to Claim 2, 120 wherein the cooled filament consisting of a polymer gel, is heated to a temperature between the swelling point of the polymer in the solvent and the melting point of the polymer and the thus-heated filament is stretched with 125 at least partial evaporation of the solvent.
 - 4. A process according to Claim 2 or Claim 3, wh rein the spun filament is cooled to below the swelling point, and then stretched at a temperatur between the swell-

130 ing point and the melting temperature.

- 5. A process according to any f Claims 1 to 4, wherein from 1 to 5 wt. % polym r solution is spun and stretch d.
- A process according to any of Claims 1
 to 5, wherein a filament containing at least 25% wt. solvent based on the polymer, is stretched.
 - 7. A process according to Claim 6, wherein the said filament contains at least
- 10 100% wt. solvent based on the polymer.
 - 8. A process according to any of Claims 1 to 7, wherein the stretching ratio is at least 5.
 - 9. A process according to Claim 8, wherein the stretching ratio is at least 10.
- 15 10. A process according to Claim 1, substantially as hereinbefore described.
 - 11. Filaments made by a process according to any of Claims 1 to 10.
- 12. Polyethylene filaments having a ten-20 sile strength of at least 1.2 GPa.

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